Mathematical Modeling in Modelica: The Art of Compressing Reality

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# Knowledge for Tomorrow

# **Equation-Based, Object-Oriented Modeling**





**Basic Model Evaluation / Simulation** 

**Multi-Domain Total System Composition** 

Code

Generation

**Object-Oriented System Composition** 

**Idealized Component Classes** 

**Fundamental Laws** 











#### Simulation Error

A fatal exception ocurred at 027:C8127 by the non-linear equation system solver. Here is a cryptic error code that is of absolutely no use: 420. Simulation has been stopped to prevent damage from your virtual universe.

\*press any key to acknowledge defeat
\*press Ctrl+Alt+Del if you think that this is any better
\*by the way, we deleted your hard-drive

Press any key to continue

# **Motivation Example: An Air Cycle**





#### **Motivation Example: An Air Cycle**



• This leads to a system with more than **200 non-linear equations** (with more than 40 iteration variables)



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## Simulation does not always work





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DLR

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#### Or taking video compression as analogy







These fundamental concepts and postulates, which cannot be further reduced logically, form the essential part of a theory, which reason cannot touch. It is the grand object of all theory to make these irreducible elements as simple and as few in numbers as possible.

- John von Neumann, "The Mathematician", 1947











[...] But simplicity certainly reflects what we mean by understanding: **understanding is compression**. So perhaps this is more about the human mind than it is about the universe.

- Gregory J Chaitin, On the intelligibility of the universe and the notions of simplicity, complexity and irreducibility, 2002 Founder of algorithmic information theory





# The problem of over-idealization



Fails to achieve instantaneous equivalent of blade element torque and air-flow momentum change



Fails to achieve instantaneous balance of power between compressor, fan and turbine



Fails to attribute kinetic energy at point of maximum stretch



#### **Over-idealization is predominant in text books**



The problem of over-idealization: idealization in components



If we idealize on the component level:

$$\lim_{\Theta \to 0} G_1(\Theta) = \lim_{\Theta \to 0} G'_1 \Theta \Rightarrow G_1 = 0 \qquad \qquad \lim_{\Theta \to 0} G_2(\Theta) = \lim_{\Theta \to 0} G'_2 \Theta \Rightarrow G_2 = 0$$

The problem of over-idealization: idealization in components



... when idealization is applied on system level.

**Over-idealization is the root of our problems.** 





**Over-idealization is the root of our problems.** 



































- Hence we end up with differential equations for the dynamic part and algebraic parts to enable compression
- Unfortunately, there is no practical way to ensure the solvability of the non-linear landscape
- Hence, I propose to aim for a different target...





- The implicit system that balances the dynamics shall be only linear, so that it has exactly one solution
- We use auxiliary dynamics (blue) to express the non-linearities that cannot be expressed by the linear part.
- We can find such forms for complex physical system.
- This form is an attractive balance between effectiveness and scalability.





# **Scalable Idealization of ThermoFluid Streams**



An effective compression is mostly about making a deliberate error.

We shall look for an error that helps to compress a lot but impacts the simulation result only by little

How to do that for thermofluid streams?





- Let us start with Euler's equation
- And bring it into integral form for an arbitrary pipe section



$$\rho \frac{\partial v_s}{\partial t} + \rho v_s \frac{\partial v_s}{\partial s} = -\frac{\partial p}{\partial s} - \frac{\partial p_{ext}}{\partial s}$$
$$\int \rho \frac{\partial v_s}{\partial t} ds + \rho \bar{v} \Delta v = -\Delta p - \Delta p_{ext}$$

• We can substitute  $v_s$  by the mass flow rate:

$$v_s = \frac{\dot{m}}{\rho A_s}$$

- Assuming the mass flow rate is constant over the stream line, we can take it out of the integral.
- The **inertance** *L* is defined as

$$L = \int \frac{1}{A_S} ds$$

• And the **inertial pressure** *r* is defined by

$$\Delta r = L \frac{d\dot{m}}{dt}$$

$$\int \rho \, \frac{\partial v_s}{\partial t} ds \, + \, \rho \, \bar{v} \, \Delta v \, = -\Delta p \, - \Delta p_{ext}$$

$$\frac{d\dot{m}}{dt}\int\frac{1}{A_s}ds + \Delta q = -\Delta p - \Delta p_{ext}$$

$$\Delta r + \Delta q = -\Delta p - \Delta p_{ext}$$



• Let us define the **steady mass flow pressure**  $\hat{p}$ 

 $p = \hat{p} + r$ 

- It is defined as the complement to the inertial pressure. Plugging in the definition...
- ... and rearranging...
- ... let us remind that q and  $p_{ext}$  depend on the thermodynamic state of the medium

$$\Delta r + \Delta q = -\Delta p - \Delta p_{ext}$$
$$\Delta q = -\Delta \hat{p} - \Delta p_{ext}$$
$$\Delta \hat{p} = \Delta p_{ext} + \Delta q$$

$$\Delta \hat{p} = \Delta p_{ext}(p, \dot{m}, ...) + \Delta q(p, \dot{m}, ...)$$





- Using  $\hat{p}$  instead of p is acceptable because:
  - when  $d\dot{m}/dt = 0$ , the error is zero
  - for gases, r is typically small
  - for liquids, the RHS is typically insensitive to r
  - many formulas (as for friction) anyway assume steady mass flow...
  - One may also say that  $\hat{p}$  and r have a different spatial resolution.
- The scheme is applicable to 96.3% of our typical Modelica use cases...

 $\Delta \hat{p} = \Delta p_{ext}(\hat{p}, \dot{m}, \dots) + \Delta q(\hat{p}, \dot{m}, \dots)$ 





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#### **A First System: Resulting Equations**



The black equations can computed straight-forward downstream What about the red equations? How to get:  $d\dot{m}_1/dt$ ,  $r_1 d\dot{m}_2/dt$ ,  $r_2$ 



# A first circuit: resulting equations



We can directly extract:

- $\cdot \frac{d\dot{m}_1}{dt} \cdot L_1 = r_1 r_A = r_1$
- $\cdot \frac{d\dot{m}_2}{dt} \cdot L_2 = r_2 r_A = r_2$

The B junction results in:

- $\hat{p}_1 + r_1 = \hat{p}_2 + r_2$ index-reduction over junction A yields:
- $d\dot{m}_1/dt = -d\dot{m}_2/dt$

from  $\dot{m}_1 + \dot{m}_2 = \dot{m}_0$ ,  $\dot{m}_0$  given

- Simple linear equation system
  - Matrix has only constant entries
  - Can be inverted upfront
- Dymola does that!

Downstream computation of thermodynamic state, assuming

Computation of mass-flow change using linear equation system over r (mostly upfront invertible)



#### **Resulting BLT Form**



• The large block at the end is linear and invertible upfront

Robus component models Robust system model

• Size of the linear block proportional to number of branches





#### **Resulting BLT Form**







#### And this method scales...



- The ENERGIZE Model describes a single-aisle more-electric aircraft
- It contains a combines electrical power and thermal management
- It allows the simulation of full flight missions under a wide variety of climatic conditions
- > 18,000 equations
- > 300 states
- faster than real-time

# **Positioning of the approach**

#### Finite Volume Approach:

- No non-linear equation systems
- Many states
- Stiffness
- High-Frequency Oscillations

# ORE

#### **DLR ThermoFluid Stream:**

- No non-linear equation systems
- Few states
- Manipulable Stiffness
- Manipulable Frequency

#### Algebraic Stream Approach:

- Complicated non-linear equation systems
- No states at all or very few
- Non-stiff / no oscillations

#### Performance

DAE



# Robustnes

#### How about mechanics?

#### **Mass-Spring Approach**

- No non-linear equation systems
- Many states
- Stiffness
- High-Frequency Oscillations



#### **Rigid Multibody**

- Few states
- Very efficient
- Non-linear equation systems
- Not feasible for contacts

#### Performance



Robustnes

#### **Reformulation of multibody dynamics**



Again all non-linear computations are explict

The implicit system, is a linear system of dimension 8. Easy to solve.

Despite the hard-impulses, we can use explicit integration method. This system was simulated with RKFIX3 at only 100Hz

Perfectly suited for hard real-time simulation (this was 300x too fast)

No need for complicated tooling to handle structural changes anymore....



#### **Reformulation of multibody dynamics**



More fun with hard contacts...

(again using explicit integration methods with fixed step size)



#### How about mechanics

#### **Mass-Spring Approach**

- No non-linear equation systems
- Many states
- Stiffness
- High-Frequency Oscillations

# Dialectic Mechanics

#### **Rigid Multibody**

- Few states
- Very efficient
- Non-linear equation systems
- Not feasible for contacts

#### Performance



Let us tackle the problem at its root...





Take home lessons I

In the Modelica Association (but also in the M&S community) we have misattributed our efforts:

- Too much focus on languages, tools, and computation

- Too little focus on modelling, underlying principles and information

There is a great potential to drastically reduce complexity in the simulation of classic physical systems but you have to deviate from classic textbook idealization



#### Take home lessons II

# Find the DLR ThermoFluid Stream Library on GitHub:

https://github.com/DLR-SR/ThermofluidStream

# **GitHub**

Feel free to contribute!!

Release	Dymola Version 2021 (64-bit) 2020-04-17	OpenModelica OpenModelica v1.19.0-dev-38-ge9f86ba1ce (64- bit) OMSimulator v2.1.1.post80-g1bf17f4-mingw	Modelon Impact
v0.1-beta	(runs and passes regression test)	$\bigotimes$	$\bigotimes$
v0.2-beta	(runs and passes regression test)	Fully compiles, mostly runs and passes regression test	(runs)
Latest main	(runs and passes regression test)	Fully compiles, mostly runs and passes regression test	(should run)

#### Papers on dialectic mechanics will be coming soon...

(and probably some sort of free library)

