

# Model-Based Optimization for a Campus District Cooling System

Kathryn Hinkelman<sup>1</sup>, Jing Wang<sup>2</sup>, Wangda Zuo<sup>1,2</sup>, Antoine Gautier<sup>3</sup>,  
Michael Wetter<sup>3</sup>, Chengliang Fan<sup>4</sup>, Nicholas Long<sup>2</sup>

<sup>1</sup> Pennsylvania State University, University Park, PA, USA

<sup>2</sup> National Renewable Energy Laboratory, Golden, CO, USA

<sup>3</sup> Lawrence Berkeley National Laboratory, Berkeley, CA, USA

<sup>4</sup> Guangzhou University, Guangzhou, China



# Overview

---

- Background and motivation
- Models for district cooling systems
- Case study
- Conclusion

# Background and Motivation

## Why District Cooling?

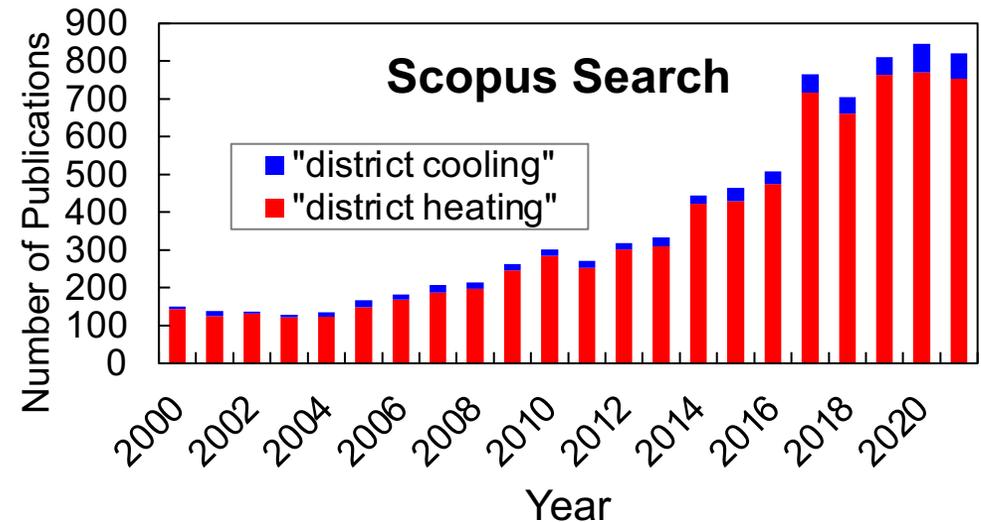
- Space cooling is growing faster than any other building end use<sup>1</sup>
- None had modeled complete district cooling systems (plant + distribution) featuring hydraulics nor waterside economizers

## Objectives

- Demonstrate how Modelica can enable complete district cooling energy analysis
- Identify investment-free energy efficiency strategies for a real-world case study
- Evaluate carbon and operational cost savings due to energy retrofits

## Gaps in Scientific Literature

- District cooling studies are generally limited

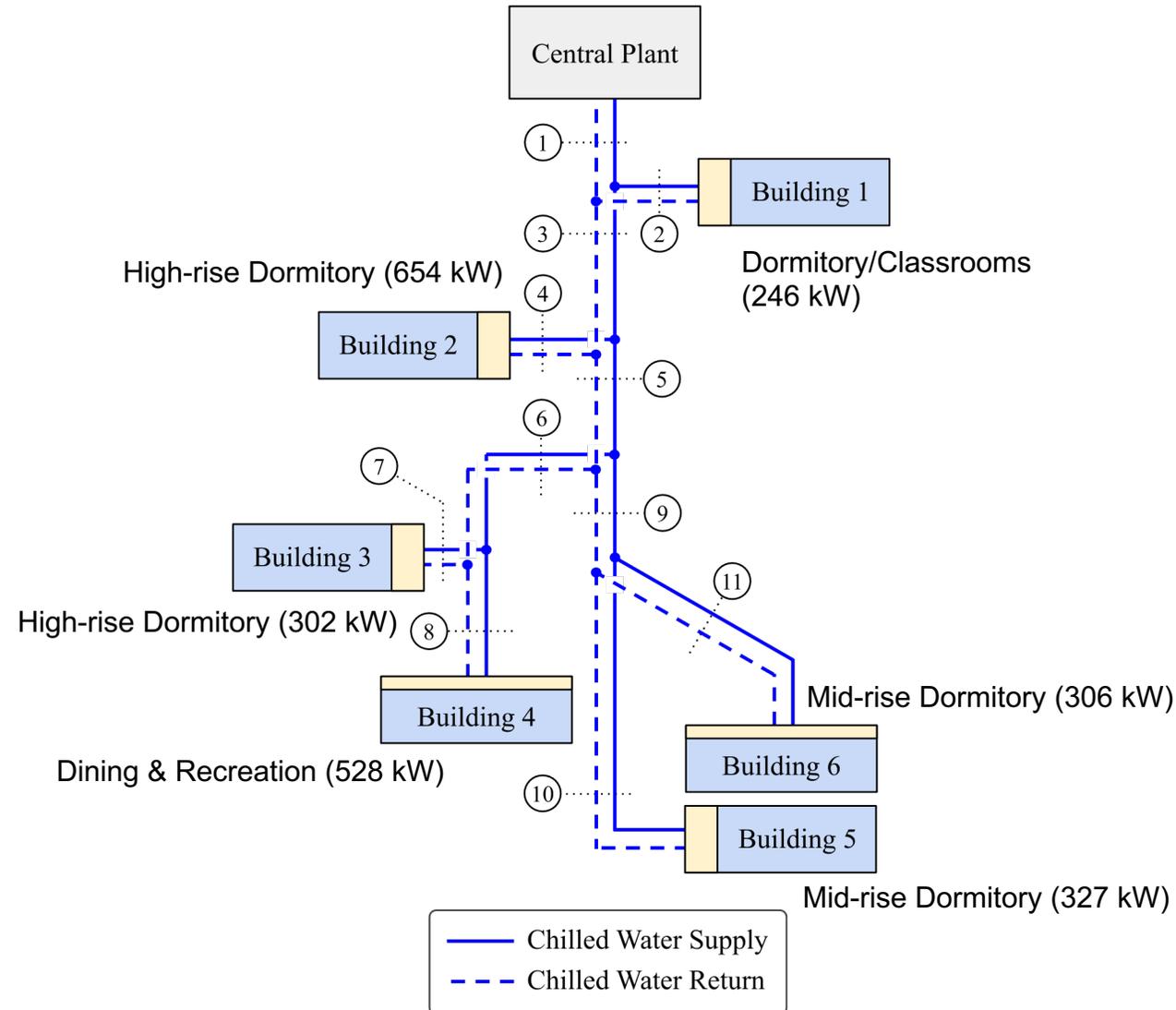


[1] International Energy Agency. 2018. The future of cooling.

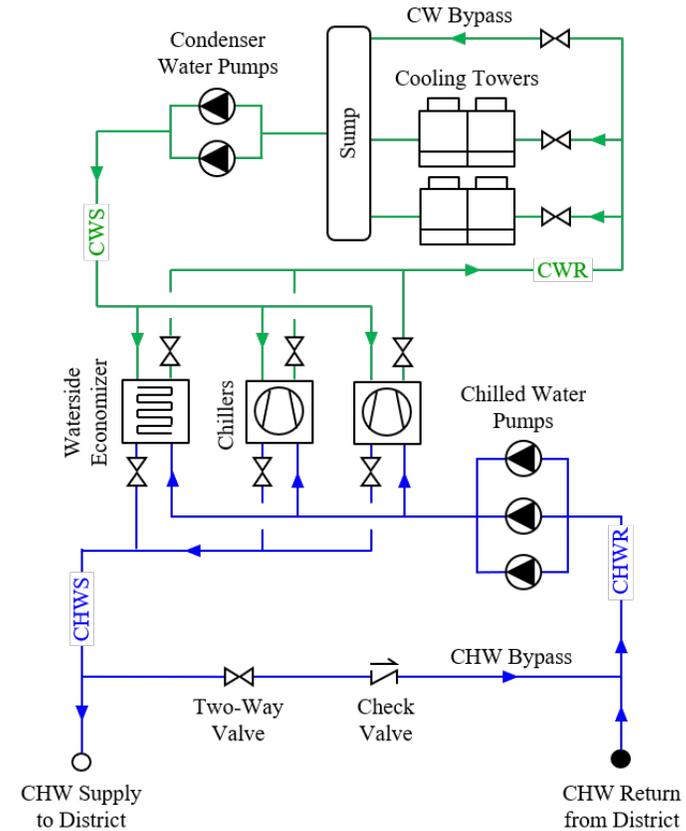
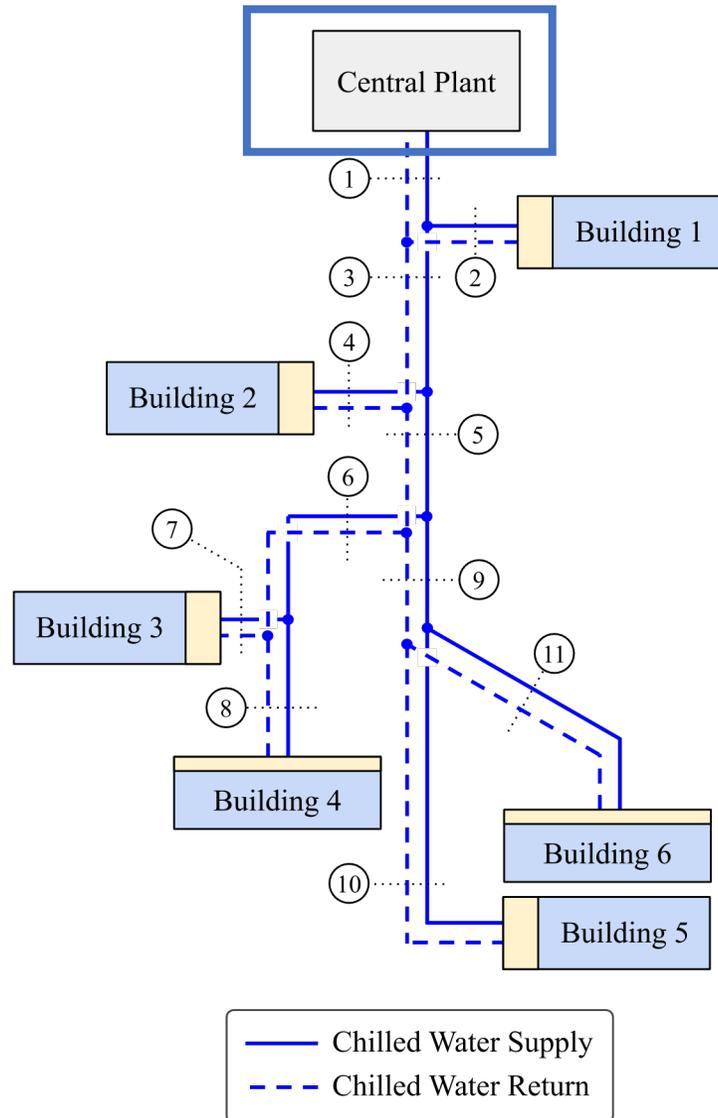
# Case Study



- A satellite campus of University of Colorado in Boulder, CO
- Six Buildings:
  - Floor area: 93,990 m<sup>2</sup> (1,011,699 ft<sup>2</sup>)
  - Peak load: 2.4 MW
- Radial network with 1.5 km pipes

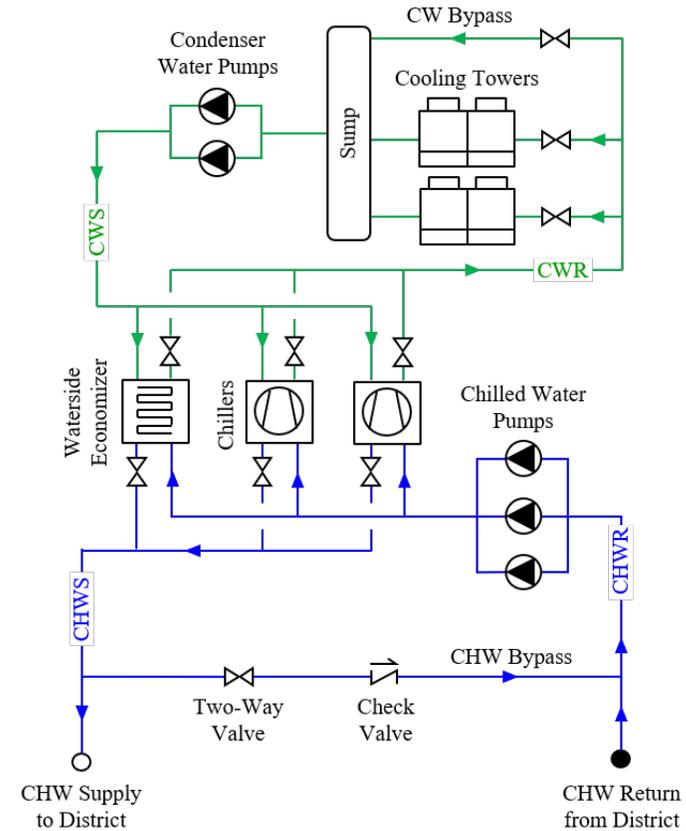
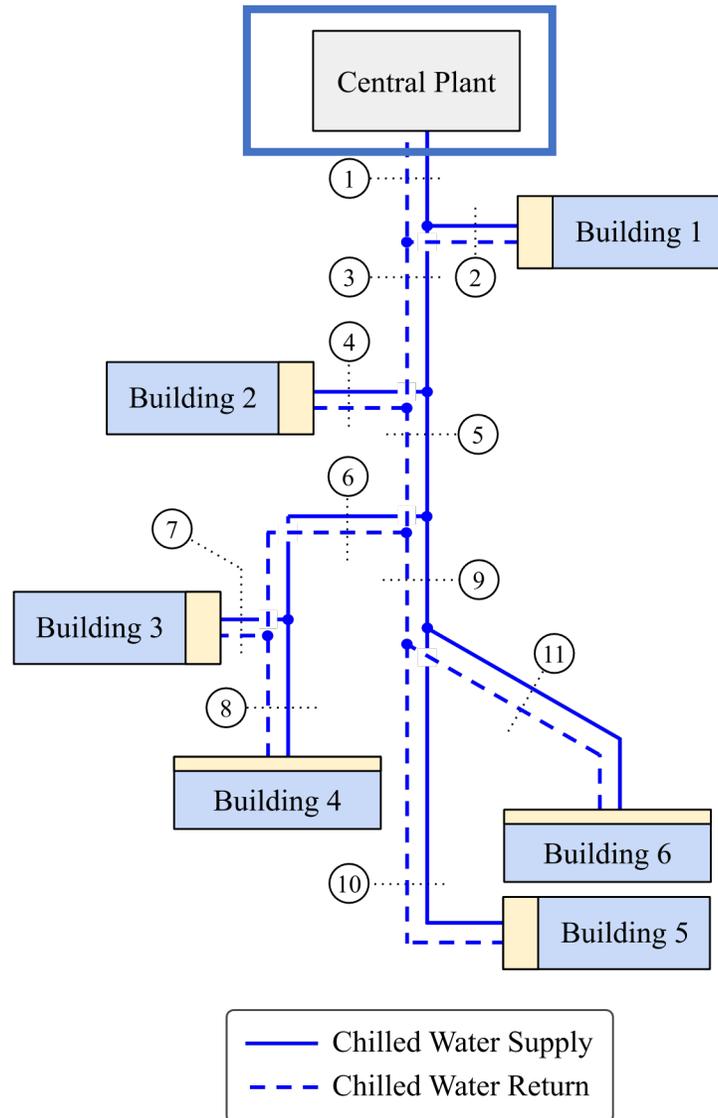


# Central Plant



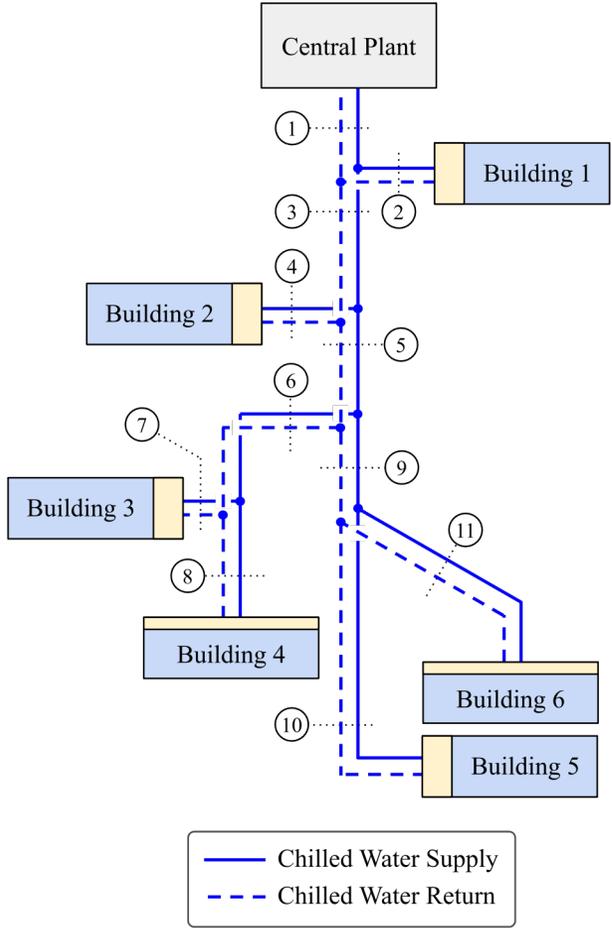
- Two single compressor chillers (2455 kW each)
- Three chilled water pump (30 kW each)
- Two condenser water pump (56 kW each)
- Non-integrated water side economizer
- Four cooling tower units (22 kW each)

# Central Plant

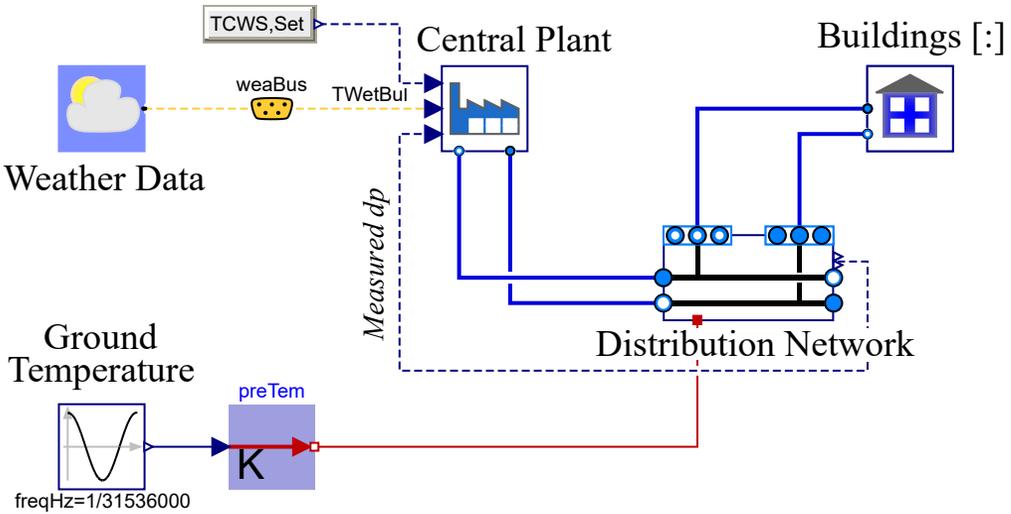


- Two single compressor chillers (2455 kW each)
- Three chilled water pump (30 kW each)
- Two condenser water pump (56 kW each)
- Non-integrated water side economizer
- Four cooling tower units (22 kW each)

# Modeling: District Cooling Systems

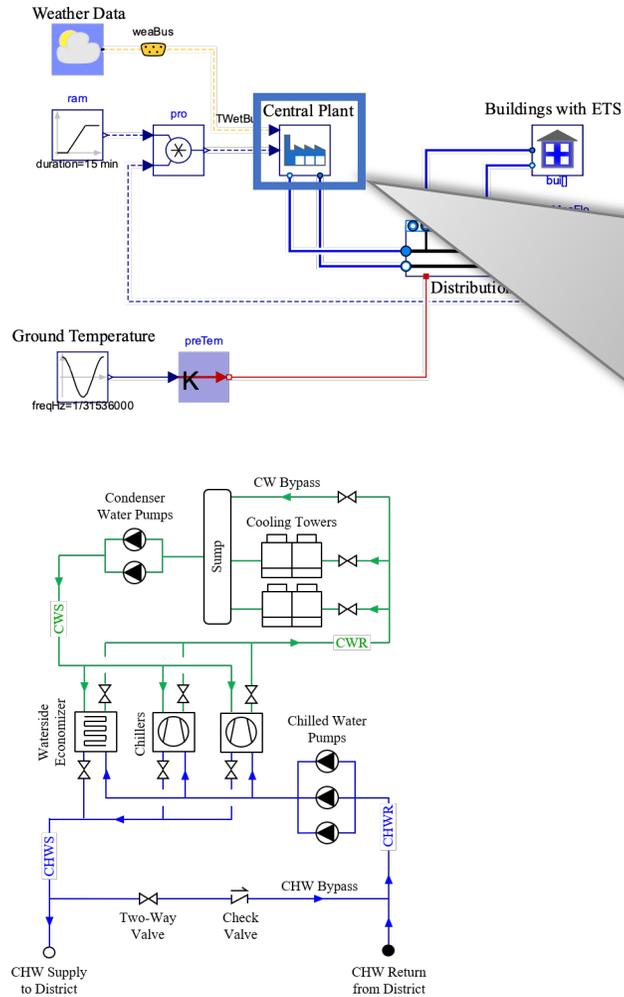


**System Schematics**

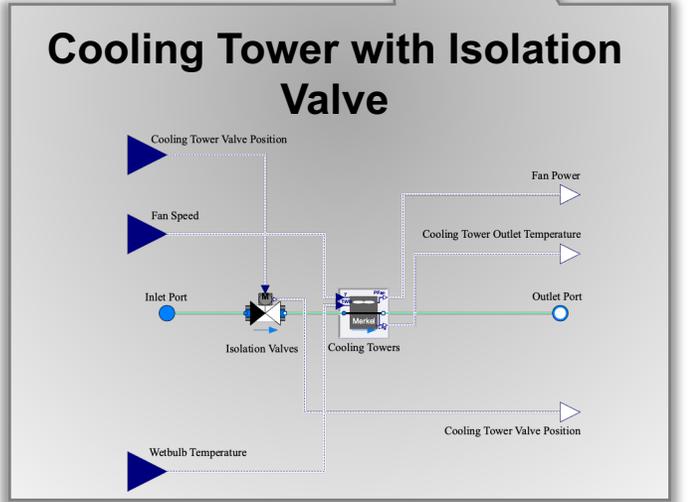
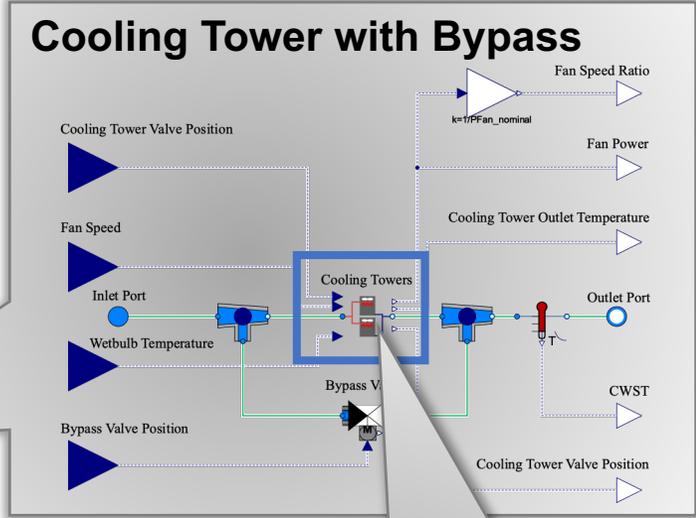
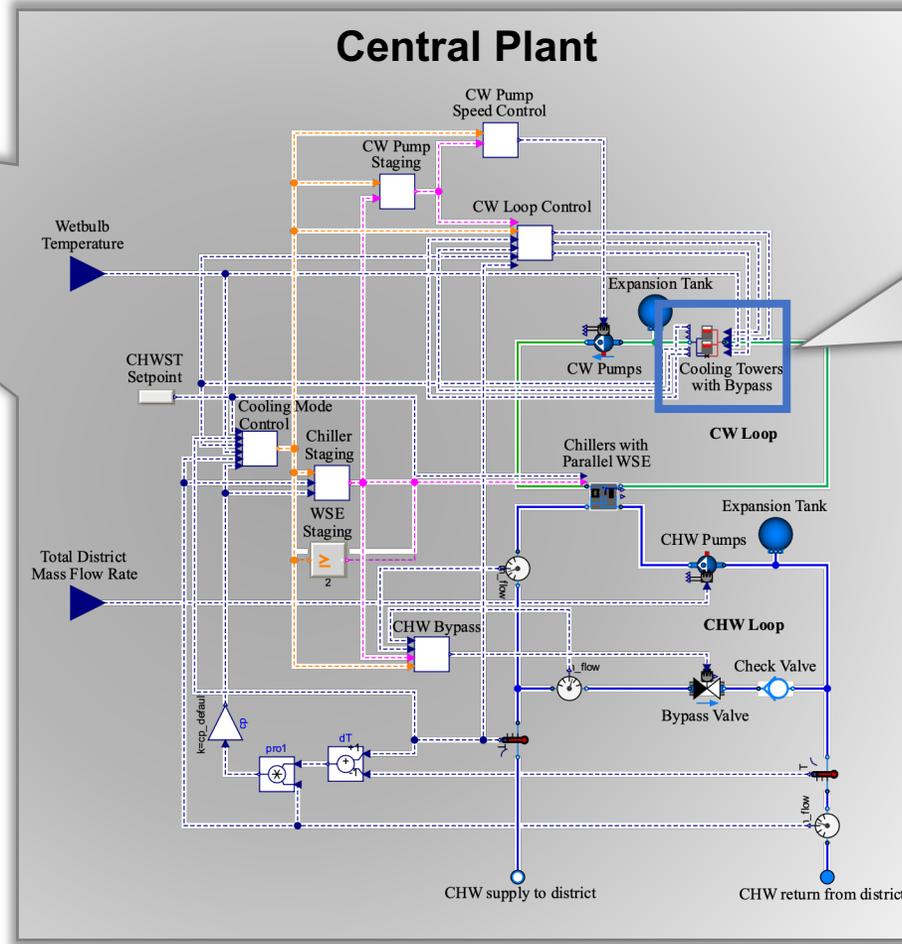


**Top-Level Model**

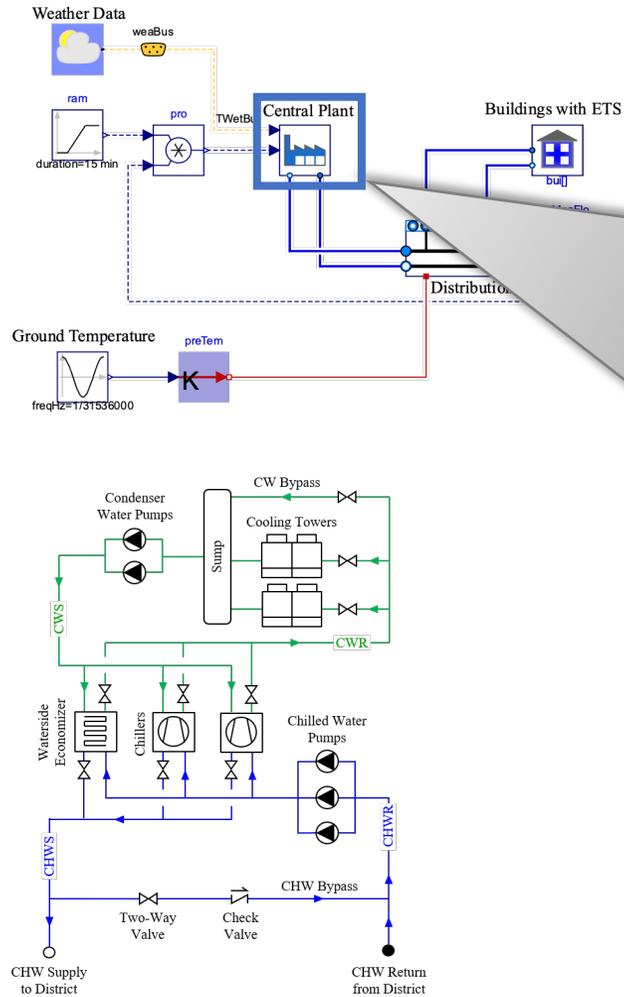
# Central Plant



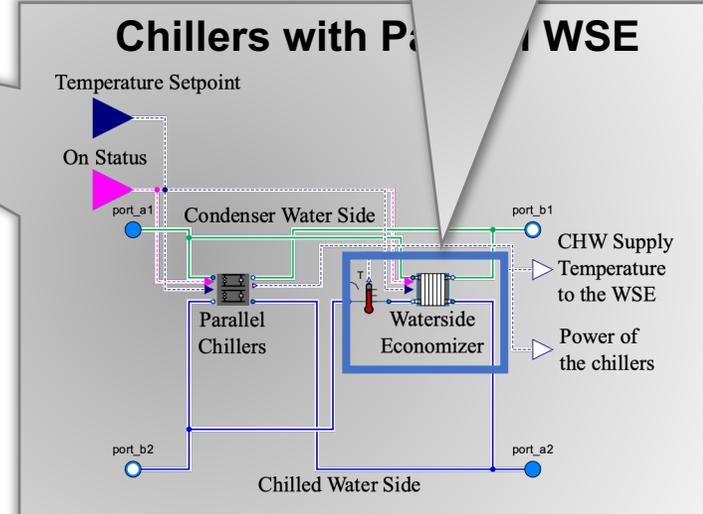
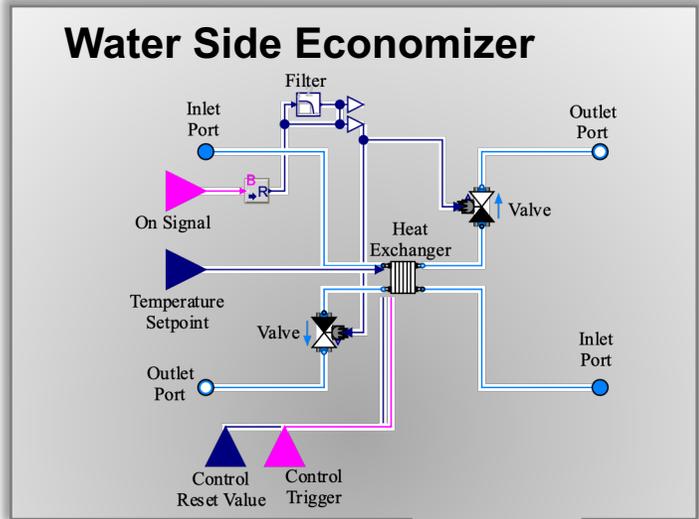
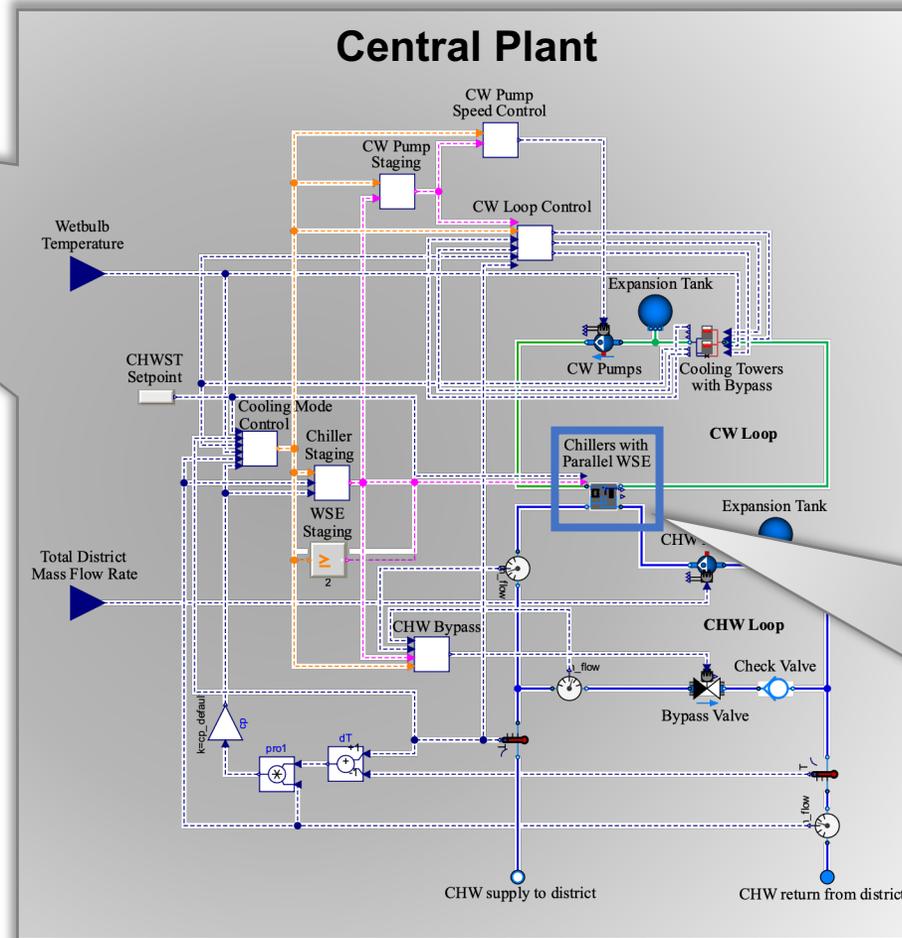
System Schematic



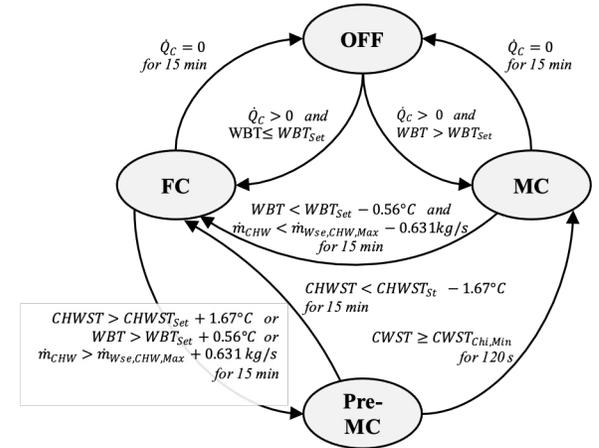
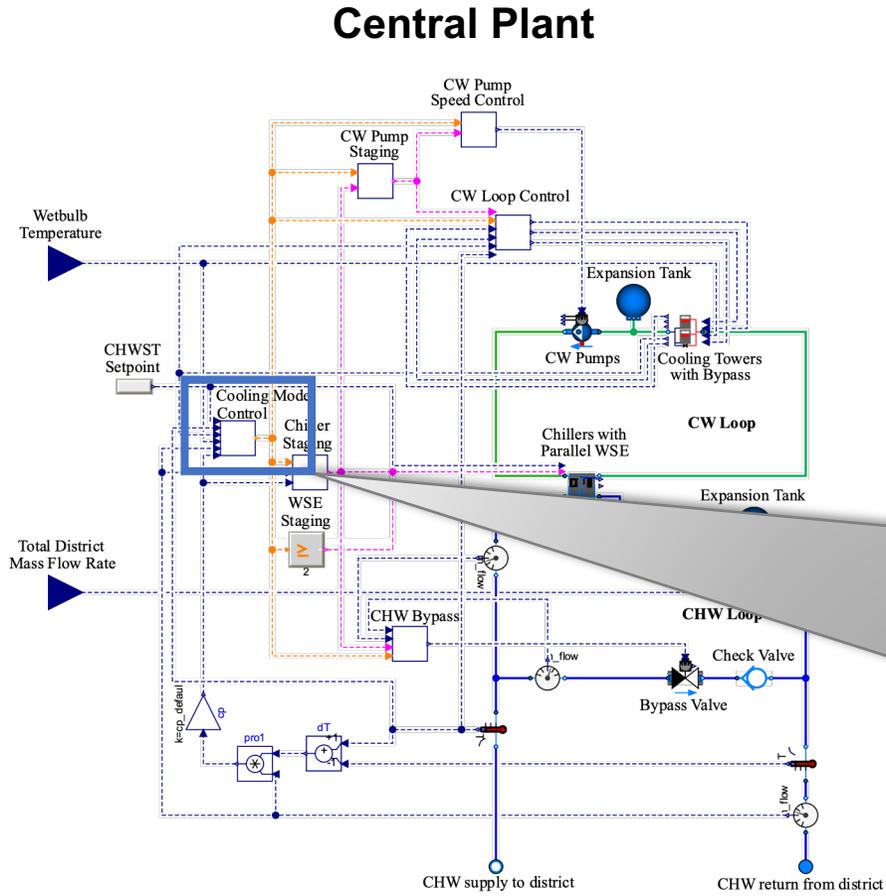
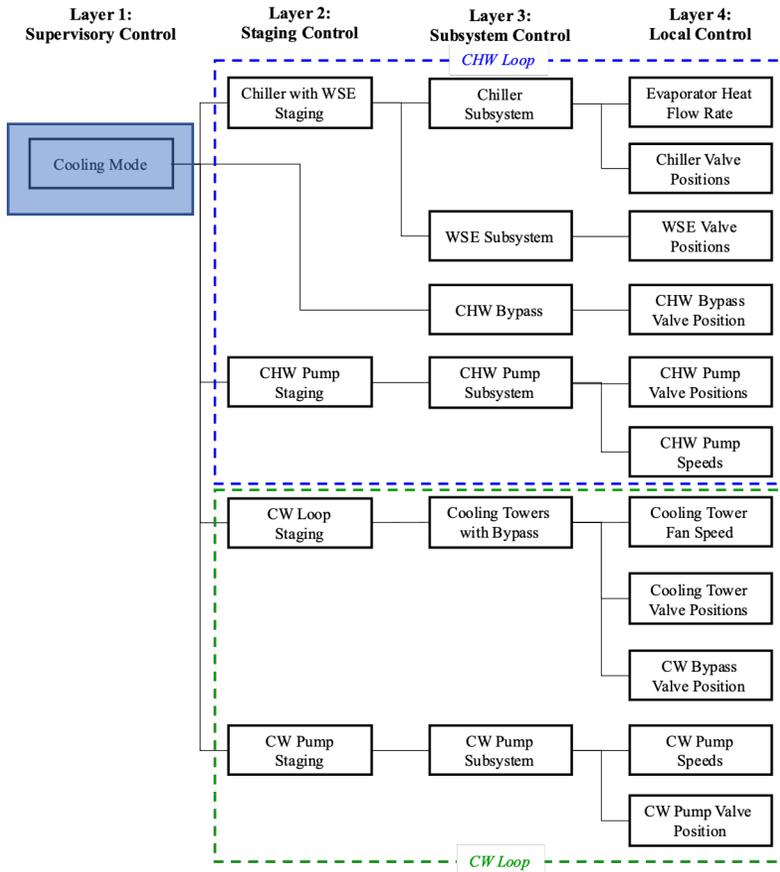
# Central Plant



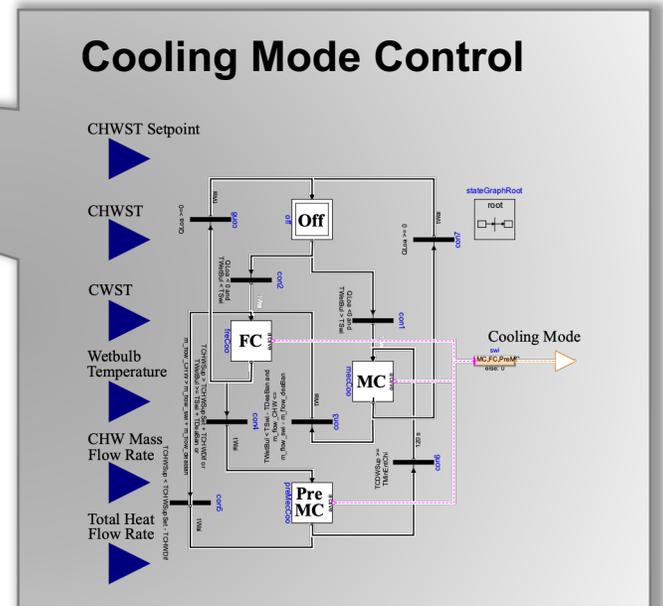
System Schematic



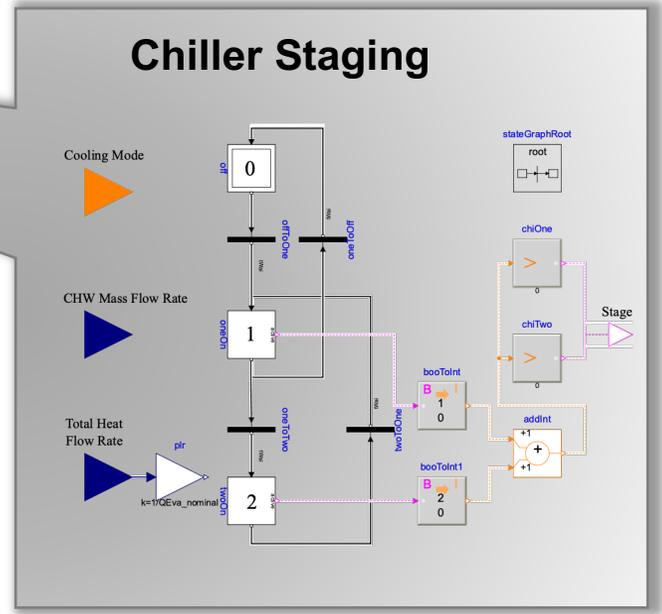
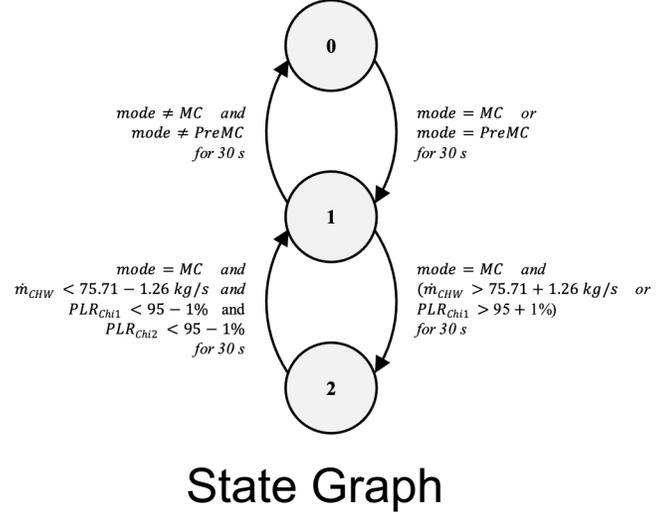
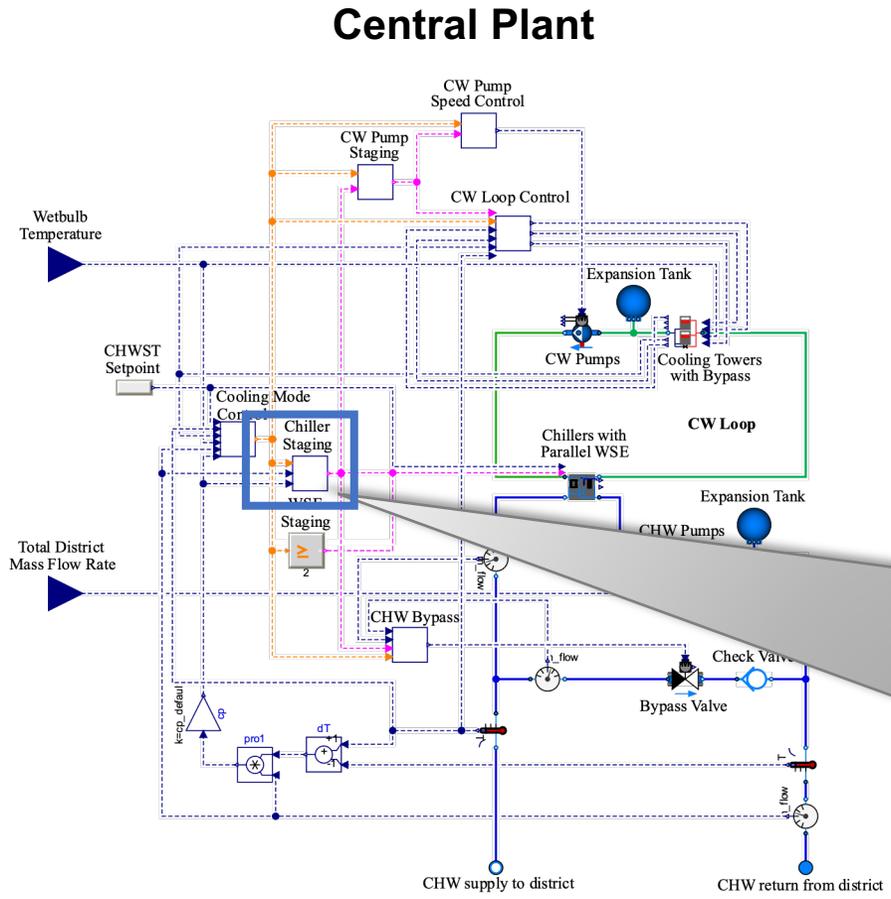
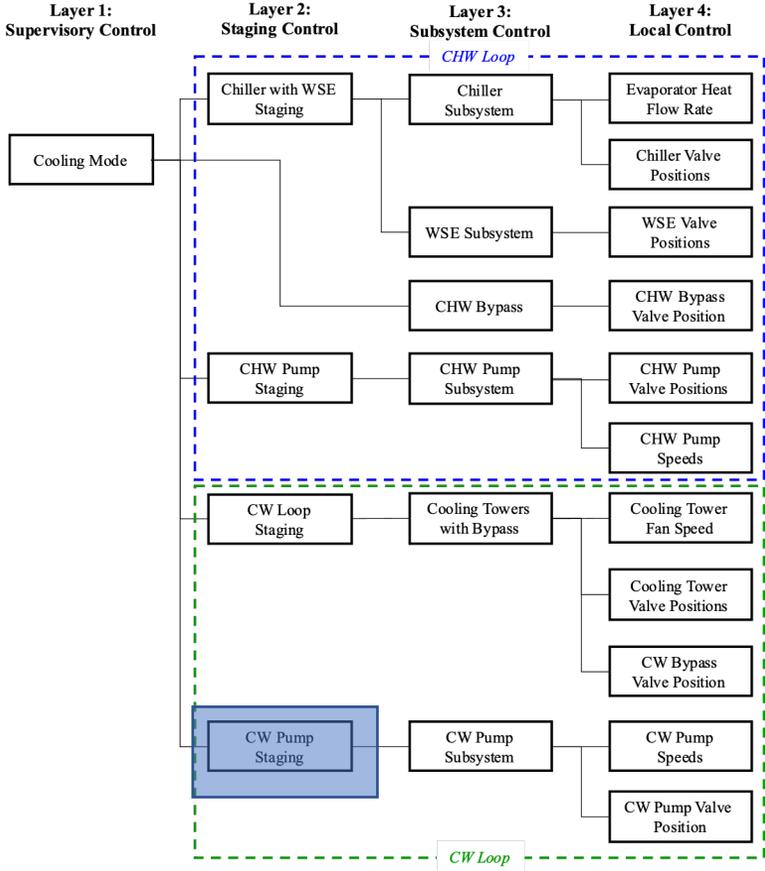
# Control Layer 1: Cooling Mode Control



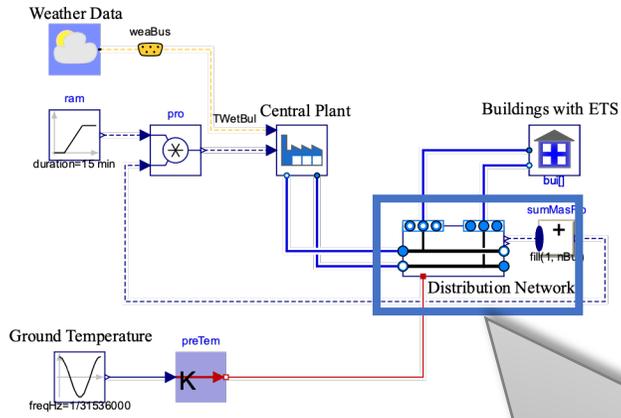
State Graph



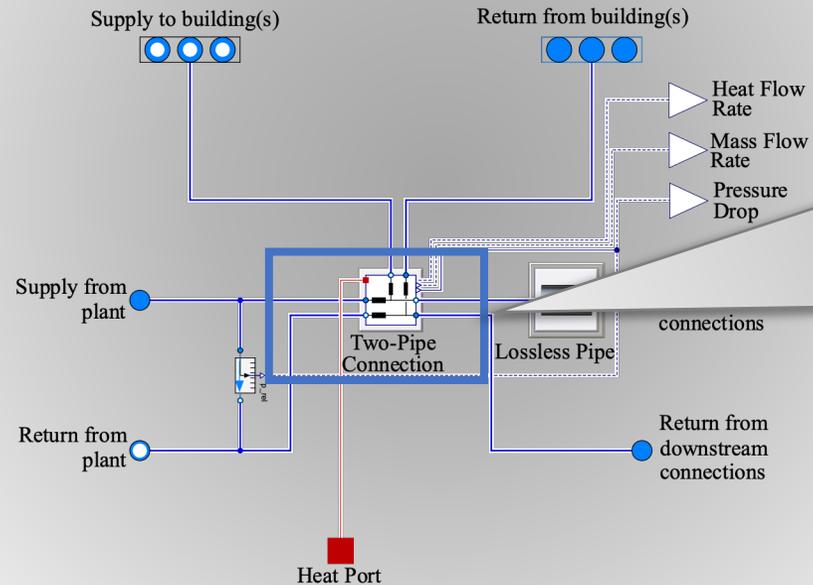
# Control Layer 2: Chiller Staging Control



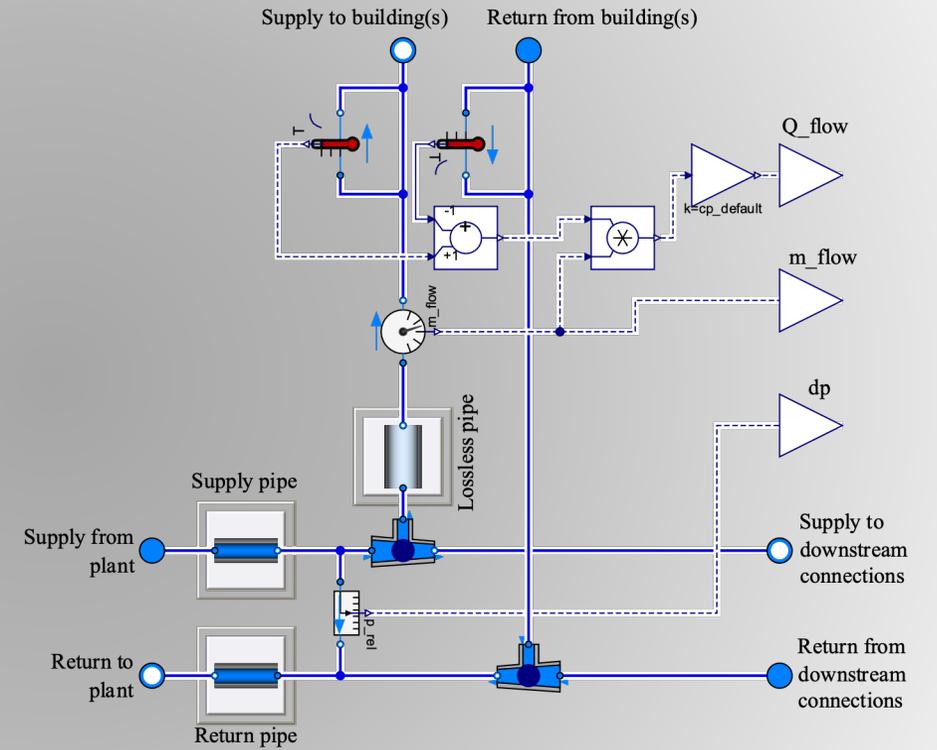
# Distribution Network



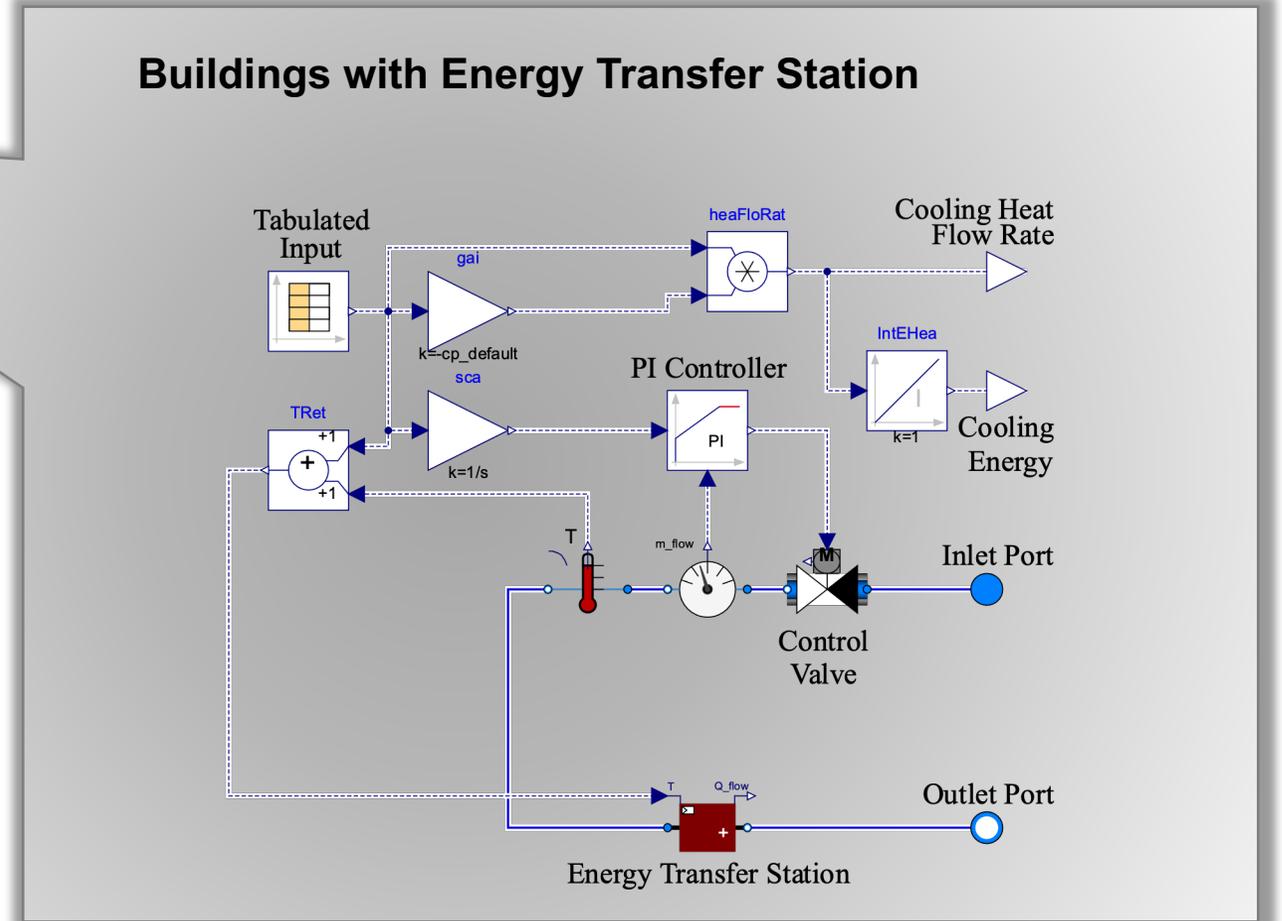
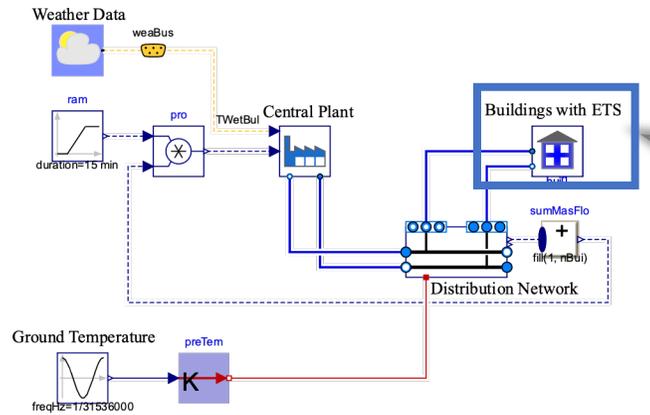
## Distribution with Two Pipes



## Connection with Two Pipes



# Buildings with Energy Transfer Station



# Validation of Models

Location	CVRMSE (%)				NMBE (%)			
	Acceptable range: [0,30%]				Acceptable range: [-10,10%]			
	$\dot{Q}_{CHW}$	$\dot{m}_{CHW}$	$T_{CHWS}$	$T_{CHWR}$	$\dot{Q}_{CHW}$	$\dot{m}_{CHW}$	$T_{CHWS}$	$T_{CHWR}$
Plant	18.8	12.9	0.3	0.2	9.7	7.4	-0.1	-0.1
Chiller	22.2	15.5	0.2	0.3	8.7	7.4	-0.1	-0.1
Building 1	2.2	0.7	0.2	0.2	0.04	1.1	0.1	0.2
Building 2	2.4	0.1	0.2	0.2	0.02	0.6	-0.01	-0.02
Building 3	3.6	0.4	0.3	0.3	0.02	0.8	0.2	0.2
Building 4	1.3	0.7	0.2	0.2	-0.02	-0.1	0.04	0.04
Building 5	1.6	0.4	0.2	0.2	0.04	0.4	0.08	0.07
Building 6	2.2	0.5	0.2	0.2	-0.05	0.5	0.01	0.01

CVRMSE (Coefficient of Variation of the Root Mean Square Error)

$$CVRMSE = \frac{\sqrt{\frac{\sum (y_i - \hat{y}_i)^2}{N-1}}}{\bar{y}}$$

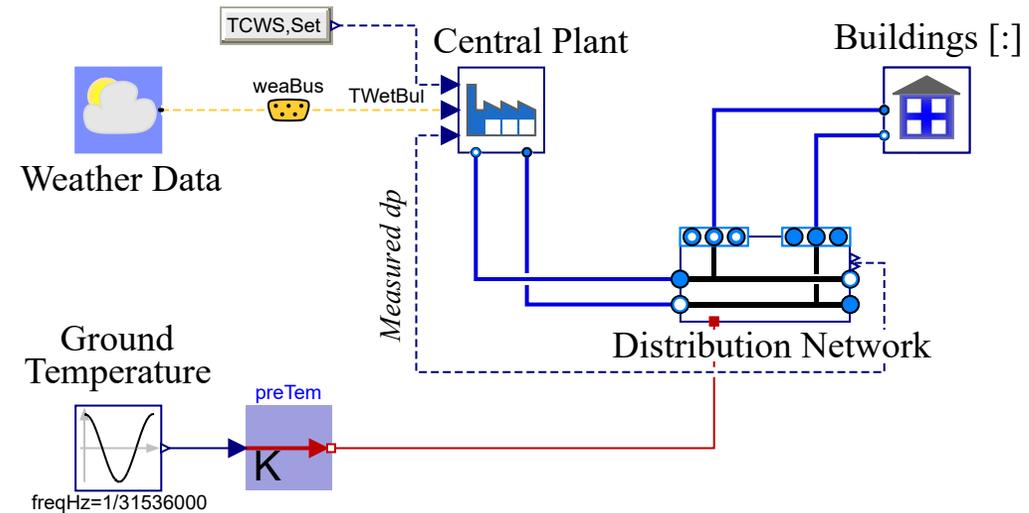
Normalized Mean Bias Error

$$NMBE = \frac{\sum (y_i - \hat{y}_i)}{(N - 1)\bar{y}}$$

Acceptable range is based on ASHRAE Guideline 14

# Model-Based System Optimization

- Condenser Water Supply Temperature
- Condenser Water Flow Rate
- Waterside Economizer



# CW Supply Temperature Setpoint Optimization

## Optimization Problem

Total plant energy

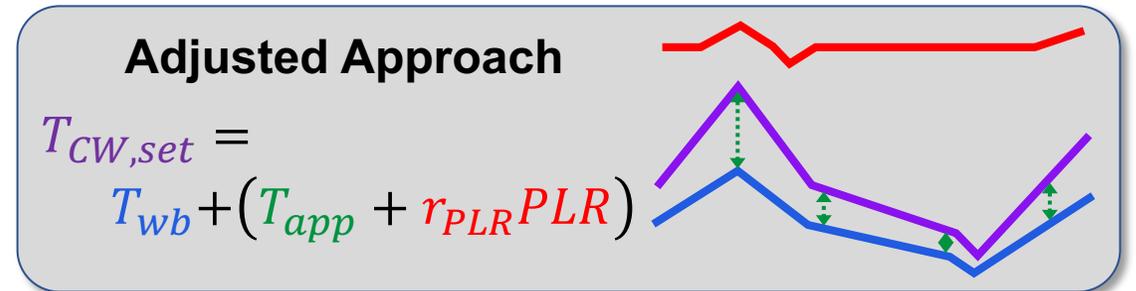
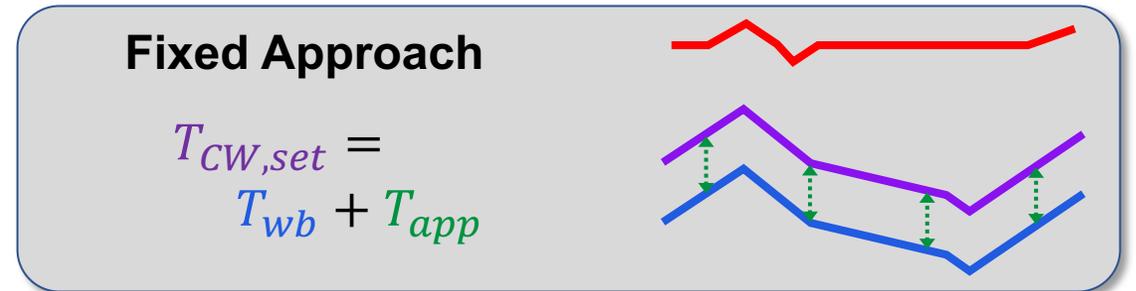
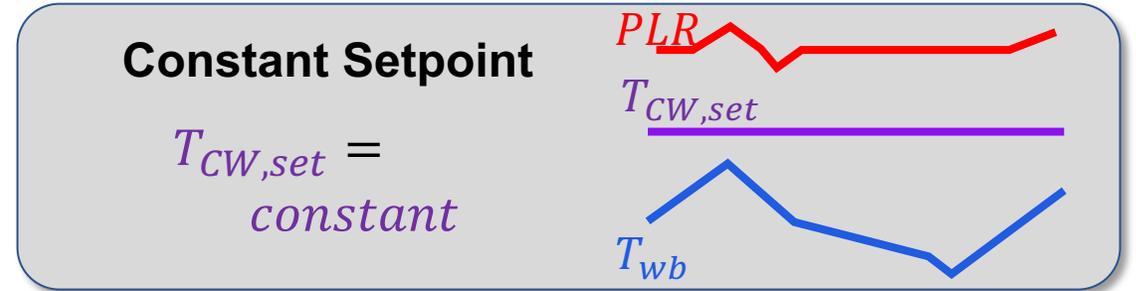
$$\min_{x \in [\underline{x}, \bar{x}]} E_{Pla,i}(T_{CW,set}(x))$$

Condenser water supply temperature setpoint

$$E_{Pla,i} = \int (P_{CH}(T_{CW,set}(x), s) + P_{CWP}(T_{CW,set}(x), s) + P_{CHWP}(T_{CW,set}(x), s) + P_{CT}(T_{CW,set}(x), s)) ds$$

Power of the:  
(chillers)  
(CW pumps)  
(CHW pumps)  
(cooling towers)

## Setpoint Methods



# Results of Optimizing Condenser Water Supply Temperature

---

$$T_{CW,set}(x_1) = x_1,$$

$$T_{CW,set}(x_1) = T_{wb} + x_1,$$

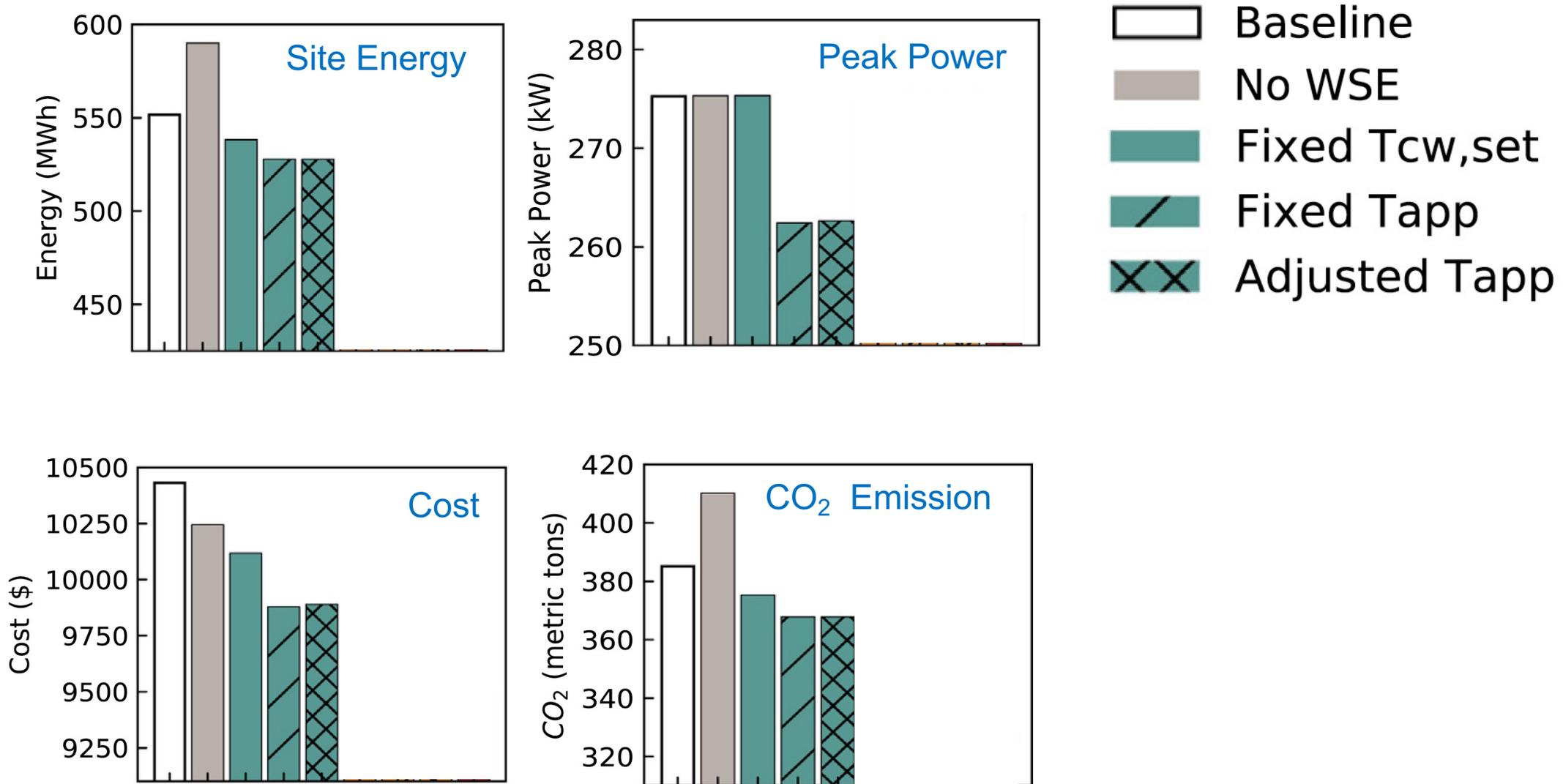
$$T_{CW,set}(x_1, x_2) = T_{wb} + x_1 + x_2 \text{ PLR}$$

**Table 4**

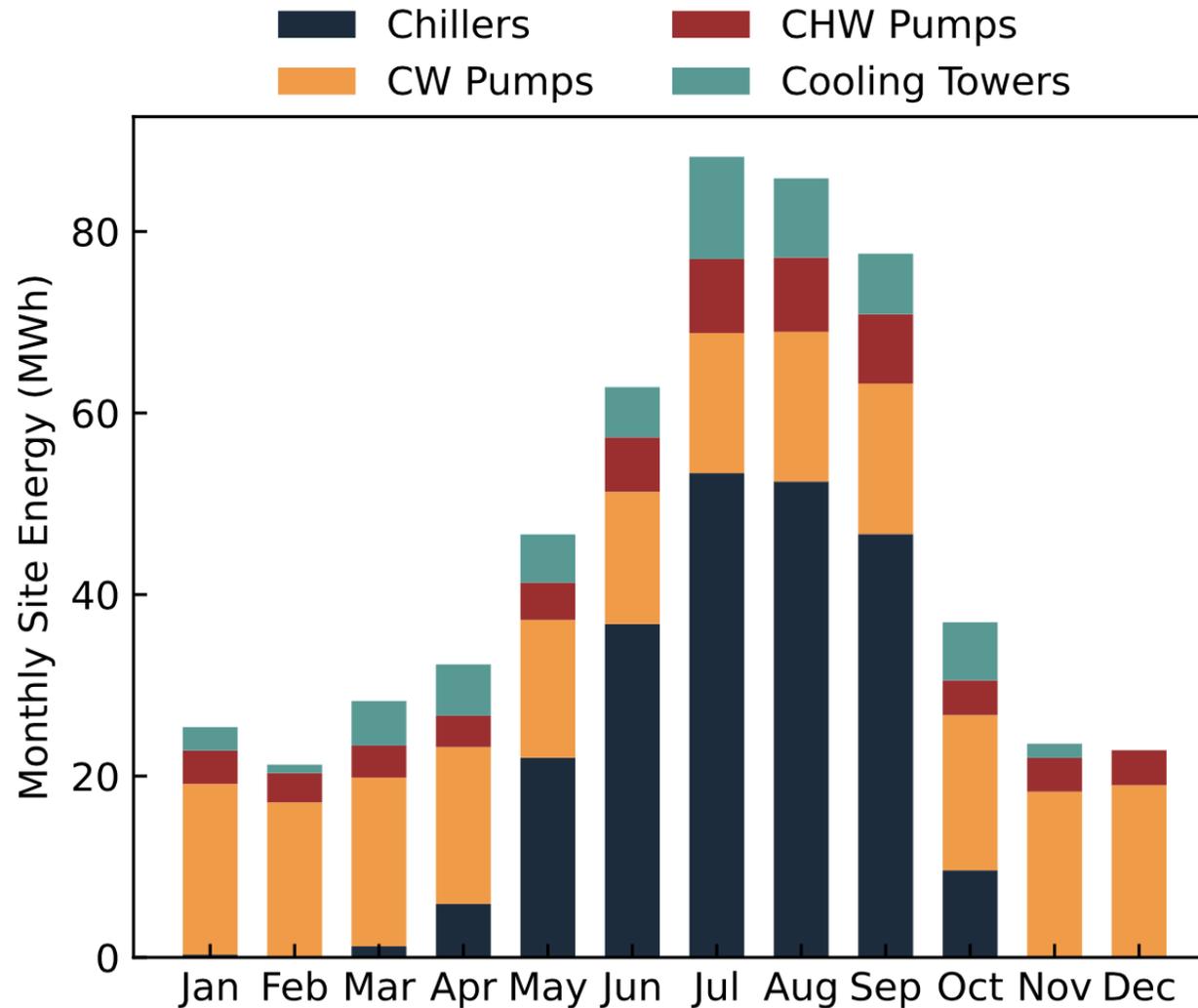
Condenser water supply temperature optimization results.

Case	Optimized $x$		Energy (MWh)	Savings (%)
	Variable	Value		
Baseline (no optimization)	$x_1$	15.6 °C	551.8	–
Fixed $T_{CW,set}$	$x_1$	18.7 °C	537.9	2.5
Fixed $T_{app}$	$x_1$	1.9 °C	527.5	4.4
Adjusted $T_{app}$	$x_1$	2.1 °C	527.5	4.4
	$x_2$	–0.44		

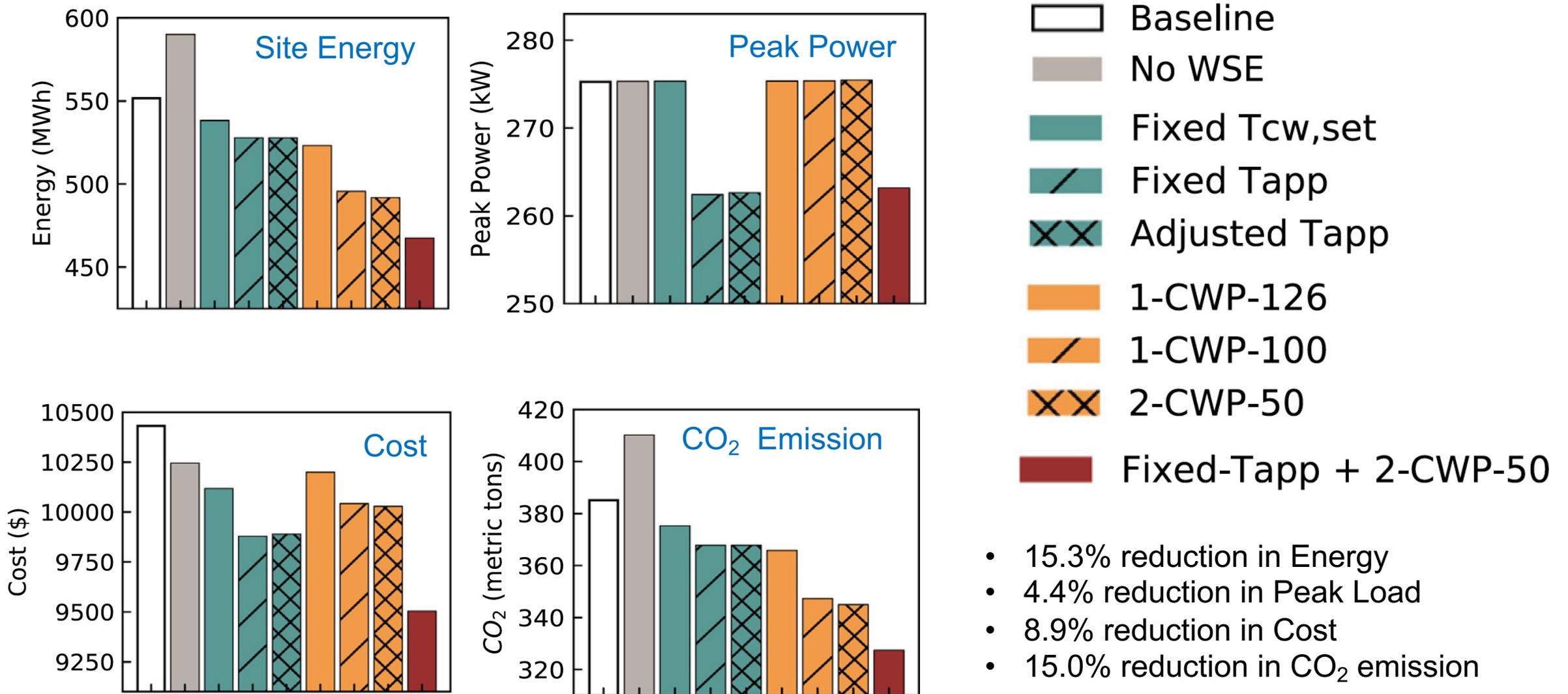
# Summary of Results



# In baseline, pumps contribute significantly to site energy use



# Summary of Results: Condenser water pump flow reduction



# Conclusion

---

- Developed open source models for the Modelica Buildings for the design and operation of district cooling systems
- Case study shows significant reductions in terms of energy (15.3%), cost (8.9%) and CO<sub>2</sub> emission (15%).

## Reference

K. Hinkelman, J. Wang, W. Zuo, A. Gautier, M. Wetter, C. Fan, N. Long. 2022. "Modelica-Based Modeling and Simulation of District Cooling Systems: A Case Study." *Applied Energy*, 311, pp.118654.

# Questions?

---

Wangda Zuo, Ph.D.

Email: [wangda.zuo@psu.edu](mailto:wangda.zuo@psu.edu)

Kathryn Hinkelman

Email: [khinkelman@psu.edu](mailto:khinkelman@psu.edu)